

# **EE6604**

## **Personal & Mobile Communications**

Week 11

Continuous Phase Modulation

Reading: 4.7, 4.8

Power Spectrum of Digitally Modulated Signals

Reading: 4.9

# Continuous Phase Modulation (CPM)

- The CPM bandpass signal is

$$\begin{aligned} s(t) &= \operatorname{Re} \left\{ A e^{j\phi(t)} e^{j2\pi f_c t} \right\} \\ &= A \cos(2\pi f_c t + \phi(t)) \end{aligned} \quad (1)$$

where the “excess phase” is

$$\phi(t) = 2\pi h \int_0^t \sum_{k=0}^{\infty} x_k h_f(\tau - kT) d\tau$$

- $h$  is the modulation index
  - $x_n \in \{\pm 1, \pm 3, \dots, \pm(M-1)\}$  are the  $M$ -ary data symbols
  - $h_f(t)$  is the “**frequency shaping pulse**” of duration  $LT$ , that is zero for  $t < 0$  and  $t > LT$ , and normalized to have an area equal to  $1/2$ . Full response CPM has  $L = 1$ , while partial response CPM has  $L > 1$ .
- The instantaneous frequency deviation from the carrier is

$$f_{\text{dev}}(t) = \frac{1}{2\pi} \frac{d\phi(t)}{dt} = h \sum_{k=0}^{\infty} x_k h_f(t - kT) .$$

# Frequency Shaping Pulses

pulse type	$h_f(t)$
$L$ -rectangular (LREC)	$\frac{1}{2LT}u_{LT}(t)$
$L$ -raised cosine (LRC)	$\frac{1}{2LT} \left[ 1 - \cos\left(\frac{2\pi t}{LT}\right) \right] u_{LT}(t)$
$L$ -half sinusoid (LHS)	$\frac{\pi}{4LT} \sin(\pi t/LT) u_{LT}(t)$
$L$ -triangular (LTR)	$\frac{1}{LT} \left( 1 - \frac{ t-LT/2 }{LT/2} \right)$

# Excess Phase and Tilted Phase

- During the time interval  $nT \leq t \leq (n+1)T$ , the **excess phase**  $\phi(t)$  is

$$\phi(t) = 2\pi h \sum_{k=0}^n x_k \beta(t - kT).$$

where the “**phase shaping pulse**” is

$$\beta(t) = \begin{cases} 0 & , t < 0 \\ \int_0^t h_f(\tau) d\tau & , 0 \leq t \leq LT \\ 1/2 & , t \geq LT \end{cases}$$

- For the case of full response CPM ( $L = 1$ ), during the time interval  $nT \leq t \leq (n+1)T$  the excess phase is

$$\phi(t) = \pi h \sum_{k=0}^{n-1} x_k + 2\pi h x_n \beta(t - nT)$$

- During the time interval  $nT \leq t \leq (n+1)T$ , the CPM “**tilted phase**” is

$$\begin{aligned} \psi(t) &= \pi h \sum_{k=0}^{n-1} x_k + 2\pi h x_n \beta(t - nT) + \pi h (M - 1) t / T \\ &= \phi(t) + \pi h (M - 1) t / T \end{aligned}$$

- Note that  $s(t)$  can be generated by replacing  $\phi(t)$  with  $\psi(t)$  and  $f_c$  by  $f_c - h(M - 1)/2T$  in (1).

# Continuous Phase Frequency Shift Keying (CPFSK)

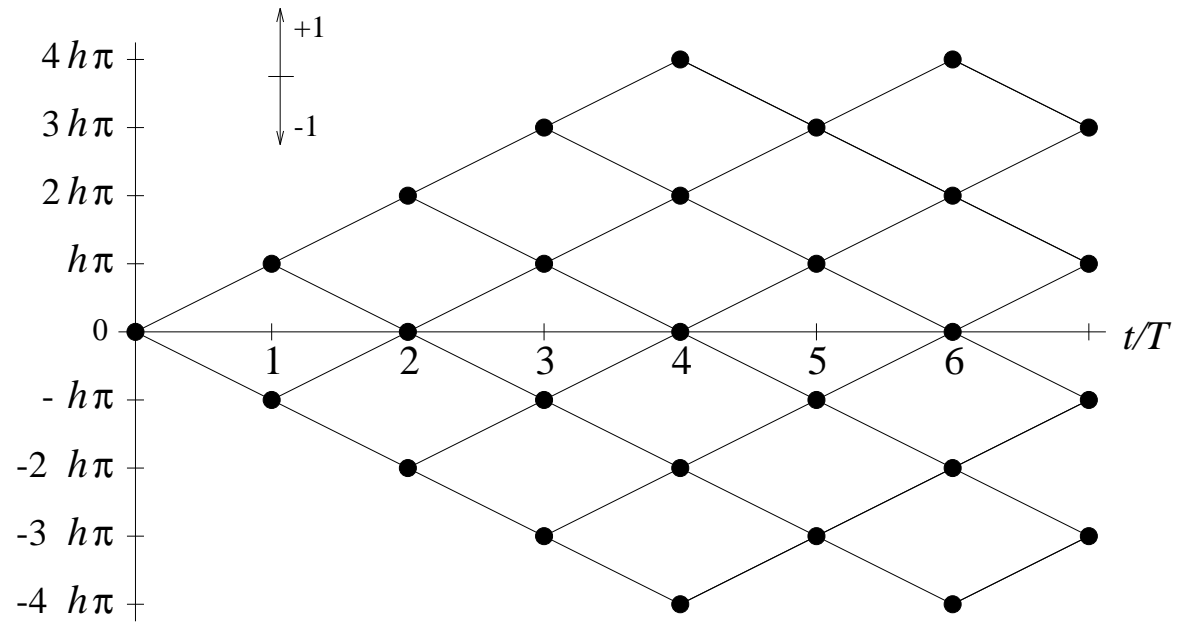
- Continuous phase frequency shift keying (CPFSK) is a special type of CPM that uses the full response REC shaping function

$$h_f(t) = \frac{1}{2T}u_T(t) = \frac{1}{2T}(u(t) - u(t - T))$$

As a result

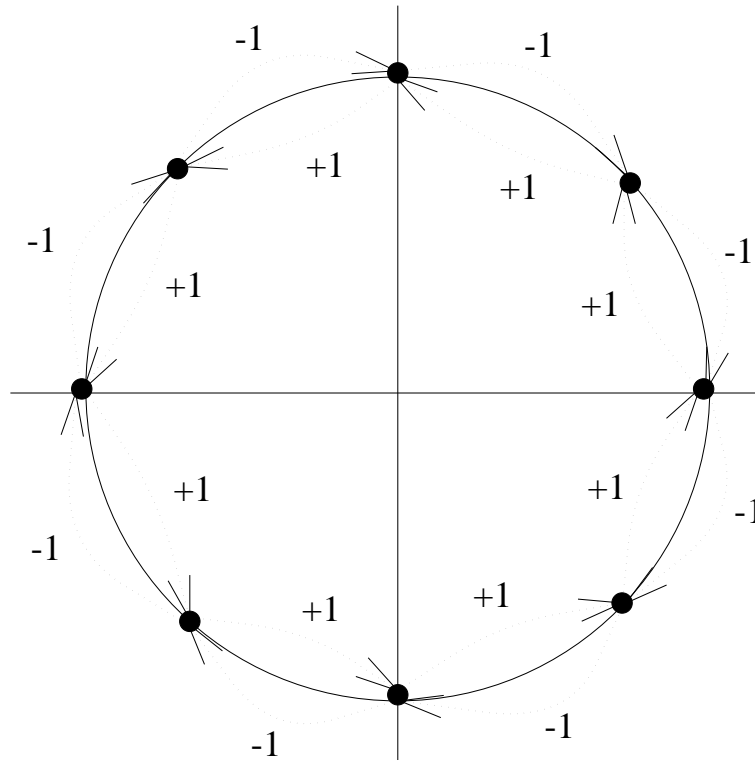
$$\beta(t) = \begin{cases} 0 & , t < 0 \\ t/2T & , 0 \leq t \leq T \\ 1/2 & , t \geq T \end{cases}$$

- Since the frequency shaping function is rectangular, the phase shaping pulse contains a linear ramp and the CPFSK excess phase trajectories are linear.



*Phase tree of binary CPFSK.*

# Phase-state Diagrams



*Phase-state diagram of CPM with  $h = 1/4$ .*

# Minimum Shift Keying (MSK)

- MSK is a special case of CPFSK, where the modulation index  $h = \frac{1}{2}$  is used.
- The phase shaping pulse is

$$\beta(t) = \begin{cases} 0 & , t < 0 \\ t/2T & , 0 \leq t \leq T \\ 1/2 & , t \geq T \end{cases}$$

- The MSK bandpass waveform is

$$s(t) = A \cos \left( 2\pi f_c t + \frac{\pi}{2} \sum_{k=0}^{n-1} x_k + \frac{t - nT}{2T} \pi x_n \right) , \quad nT \leq t \leq (n+1)T$$

- The **excess phase** on the interval  $nT \leq t \leq (n+1)T$  is

$$\phi(t) = \frac{\pi}{2} \sum_{k=0}^{n-1} x_k + \frac{t - nT}{2T} \pi x_n$$

- The **tilted phase** on the interval  $nT \leq t \leq (n+1)T$  is

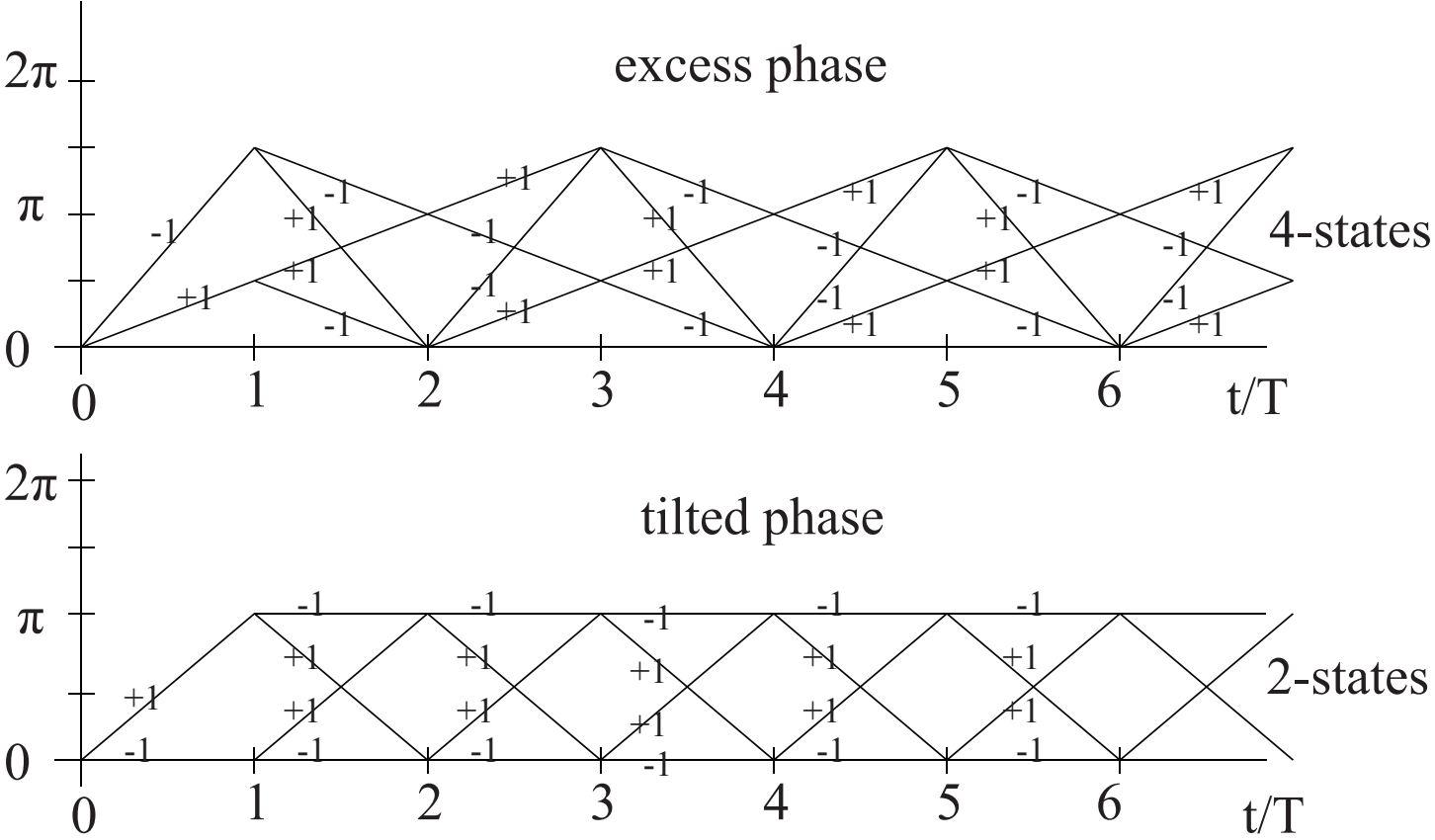
$$\psi(t) = \phi(t) + \frac{\pi t}{2T}$$

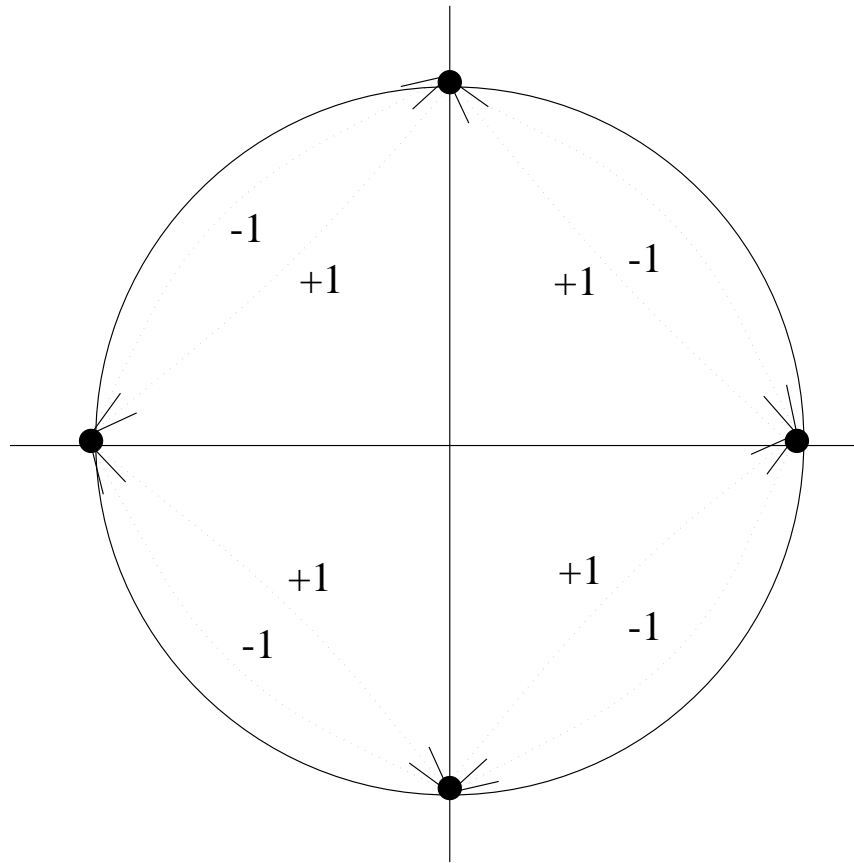
- Combining the above two equations, we have

$$\psi((n+1)T) = \psi(nT) + \frac{\pi}{2}(1 + x_n)$$



# Excess Phase and Tilted Phase for Minimum Shift Keying (MSK)





*Phase state diagram for MSK signals.*

# Linearized Representation of MSK

- An interesting representation for MSK waveforms can be obtained by using Laurent's decomposition to express the MSK complex envelope in the quadrature form

$$\tilde{s}(t) = A \sum_n b(t - 2nT, \mathbf{x}_n) ,$$

where

$$b(t, \mathbf{x}_n) = \hat{x}_{2n+1} h_a(t - T) + j \hat{x}_{2n} h_a(t)$$

and where  $\mathbf{x}_n = (\hat{x}_{2n+1}, \hat{x}_{2n})$ ,

$$\hat{x}_{2n} = \hat{x}_{2n-1} x_{2n} \tag{2}$$

$$\hat{x}_{2n+1} = -\hat{x}_{2n} x_{2n+1} \tag{3}$$

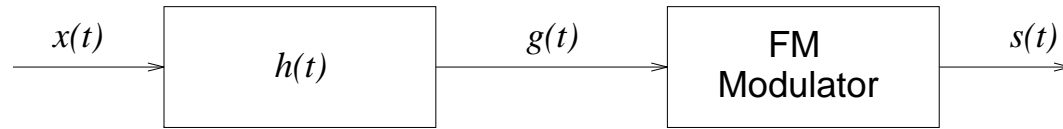
$$\hat{x}_{-1} = 1 \tag{4}$$

and

$$h_a(t) = \sin\left(\frac{\pi t}{2T}\right) u_{2T}(t) .$$

- The sequences,  $\{\hat{x}_{2n}\}$  and  $\{\hat{x}_{2n+1}\}$ , are independent binary symbol sequences taking on elements from the set  $\{-1, +1\}$ .
- The symbols  $\hat{x}_{2n}$  and  $\hat{x}_{2n+1}$  are transmitted on the quadrature branches with a half-sinusoid (HS) amplitude shaping pulse of duration  $2T$  seconds and an offset of  $T$  seconds.

# Gaussian MSK (GMSK)



*Gaussian Pre-modulation filtered MSK (GMSK).*

- With MSK the modulating signal is

$$x(t) = \frac{1}{2T} \sum_{n=-\infty}^{\infty} x_n u_T(t - nT)$$

- The bandwidth of  $\tilde{s}(t)$  depends on the bandwidth of  $x(t)$  and the modulation index  $h$ . For GMSK  $h = 1/2$ .
- We filter  $x(t)$  with a low-pass filter to remove high frequency content prior to modulation, i.e., we use the filtered pulse  $g(t) = x(t) * h(t)$ .
- For GMSK, the low-pass filter transfer function is

$$H(f) = \exp \left\{ - \left( \frac{f}{B} \right)^2 \frac{\ln 2}{2} \right\}$$

where  $B$  is the 3 dB filter bandwidth.

*Gaussian Pre-modulation filtered MSK (GMSK).*

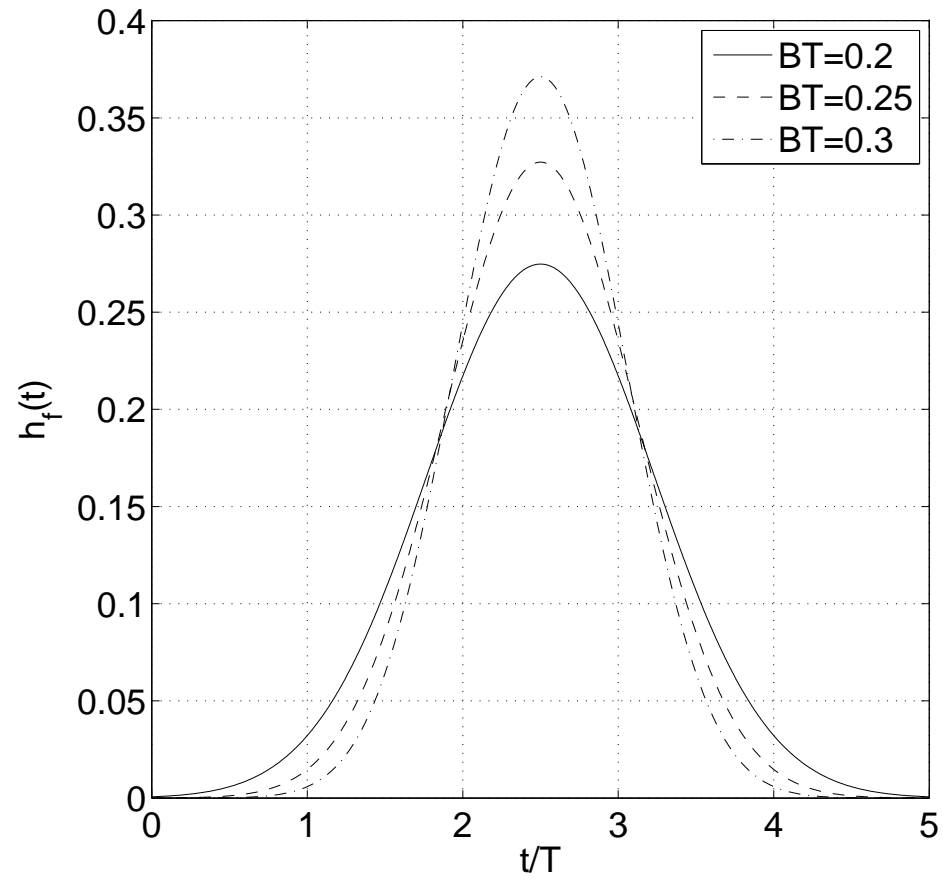
- A rectangular pulse  $\text{rect}(t/T) = u_T(t + T/2)$  transmitted through this Gaussian low-pass filter yields the GMSK frequency shaping pulse

$$\begin{aligned}
 h_f(t) &= \frac{1}{2T} \sqrt{\frac{2\pi}{\ln 2}} (BT) \int_{t/T-1/2}^{t/T+1/2} \exp \left\{ -\frac{2\pi^2 (BT)^2 x^2}{\ln 2} \right\} dx \\
 &= \frac{1}{2T} \left[ Q \left( \frac{t/T - 1/2}{\sigma} \right) - Q \left( \frac{t/T + 1/2}{\sigma} \right) \right]
 \end{aligned}$$

where

$$\begin{aligned}
 Q(\alpha) &= \int_{\alpha}^{\infty} \frac{1}{\sqrt{2\pi}} e^{-x^2/2} dx \\
 \sigma^2 &= \frac{\ln 2}{4\pi^2 (BT)^2} .
 \end{aligned}$$

- The total pulse area is  $\int_{-\infty}^{\infty} h_f(t) dt = 1/2$  and, therefore, the total contribution to the excess phase for each data symbol is  $\pm\pi/2$  radians.



*GMSK frequency shaping pulse for various normalized filter bandwidths  $BT$ .*

- The GMSK phase shaping pulse is

$$\beta(t) = \int_{-\infty}^t h_f(t) dt = \frac{1}{2} \left( G \left( \frac{t}{T} + \frac{1}{2} \right) - G \left( \frac{t}{T} - \frac{1}{2} \right) \right)$$

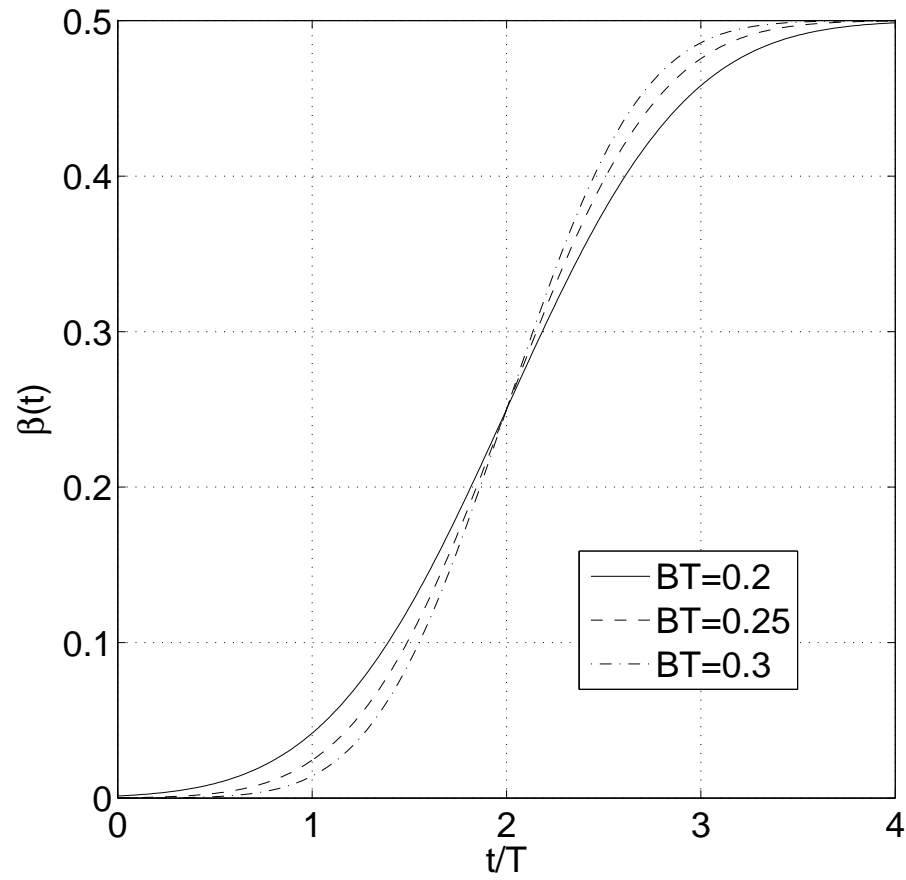
where

$$G(x) = x \Phi \left( \frac{x}{\sigma} \right) + \frac{\sigma}{\sqrt{2\pi}} e^{-\frac{x^2}{2\sigma^2}} ,$$

and

$$\Phi(\alpha) = \int_{-\infty}^{\alpha} \frac{1}{\sqrt{2\pi}} e^{-x^2/2} dx$$

- Observe that  $\beta(\infty) = 1/2$  and, therefore, the total contribution to the excess phase for each data symbol remains at  $\pm\pi/2$  as mentioned earlier.



*GMSK phase shaping pulse for various normalized filter bandwidths  $BT$ .*



- The excess phase change over the interval from  $-T/2$  to  $T/2$  is

$$\phi(T/2) - \phi(-T/2) = x_0\beta_0(T) + \sum_{\substack{n=-\infty \\ n \neq 0}}^{\infty} x_n\beta_n(T)$$

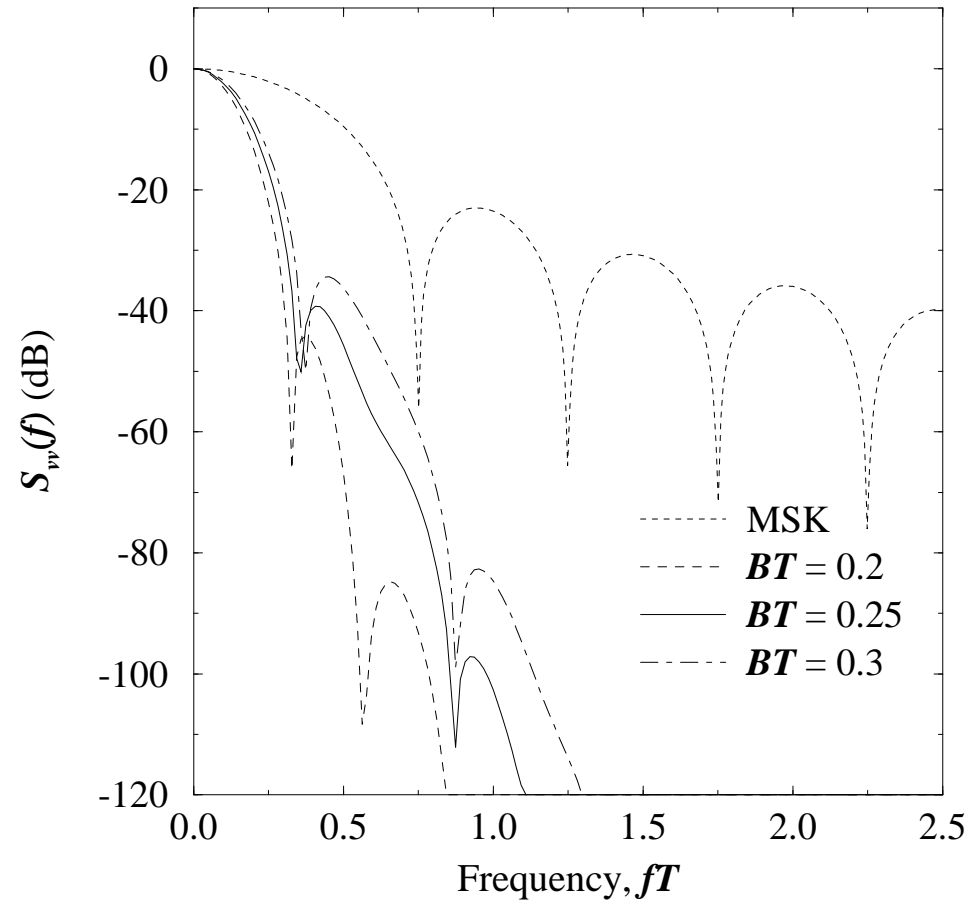
where

$$\beta_n(T) = \int_{-T/2-nT}^{T/2-nT} h_f(\nu) d\nu .$$

and

$$h_f(t) = \frac{1}{2T} \left[ Q \left( \frac{t/T - 1/2}{\sigma} \right) - Q \left( \frac{t/T + 1/2}{\sigma} \right) \right]$$

- The first term,  $x_0\beta_0(T)$  is the desired term, and the second term,  $\sum_{\substack{n=-\infty \\ n \neq 0}}^{\infty} x_n\beta_n(T)$ , is the intersymbol interference (ISI) introduced by the Gaussian low-pass filter.
- **Conclusion:** GMSK trades off power efficiency (due to the induced ISI) for a greatly improved bandwidth efficiency.
  - the loss in power efficiency can be recovered by using an equalizer in the receiver to mitigate the induced ISI.



*Power spectral density of GMSK with various normalized filter bandwidths  $BT$ .*

# Linearized Gaussian Minimum Shift Keying (LGMSK)

- Laurent showed that any binary partial response CPM signal can be represented exactly as a linear combination of  $2^{L-1}$  partial-response pulse amplitude modulated (PAM) signals, viz.,

$$\tilde{s}(t) = \sum_{n=0}^{\infty} \sum_{p=0}^{2^{L-1}-1} e^{j\pi h \alpha_{n,p}} c_p(t - nT),$$

where

$$c_p(t) = c(t) \prod_{n=1}^{L-1} c(t + (n + L\varepsilon_{n,p})T),$$

$$\alpha_{n,p} = \sum_{m=0}^n x_m - \sum_{m=1}^{L-1} x_{n-m} \varepsilon_{m,p},$$

and  $\varepsilon_{n,p} \in \{0, 1\}$  are the coefficients of the binary representation of the index  $p$ , i.e.,

$$p = \varepsilon_{0,p} + 2\varepsilon_{1,p} + \cdots + 2^{L-2}\varepsilon_{L-2,p} .$$

- The basic signal pulse  $c(t)$  is

$$c(t) = \begin{cases} \frac{\sin(2\pi h \beta(t))}{\sin \pi h} & , \quad 0 \leq t < LT \\ \frac{\sin(\pi h - 2\pi h \beta(t-LT))}{\sin \pi h} & , \quad LT \leq t < 2LT \\ 0 & , \quad \text{otherwise} \end{cases} ,$$

where  $\beta(t)$  is the CPM phase shaping function.

# Linearized Gaussian Minimum Shift Keying (LGMSK)

- Note that the GMSK frequency shaping pulse spans  $L = 3$  to  $L = 4$  symbol periods for practical values of  $BT$ .
- Often the pulse  $c_0(t)$  contains most of the signal energy, so the  $p = 0$  term in can provide a good approximation to the CPM signal. Numerical analysis can show that the pulse  $c_0(t)$  contains 99.83% of the energy and, therefore, we can derive a linearized GMSK waveform by using only  $c_0(t)$  and neglecting the other pulses.
- This yields the waveform

$$\tilde{s}(t) = \sum_{n=0}^{\infty} e^{j\pi h \alpha_{n,0}} c_0(t - nT),$$

where, with  $L = 4$ ,

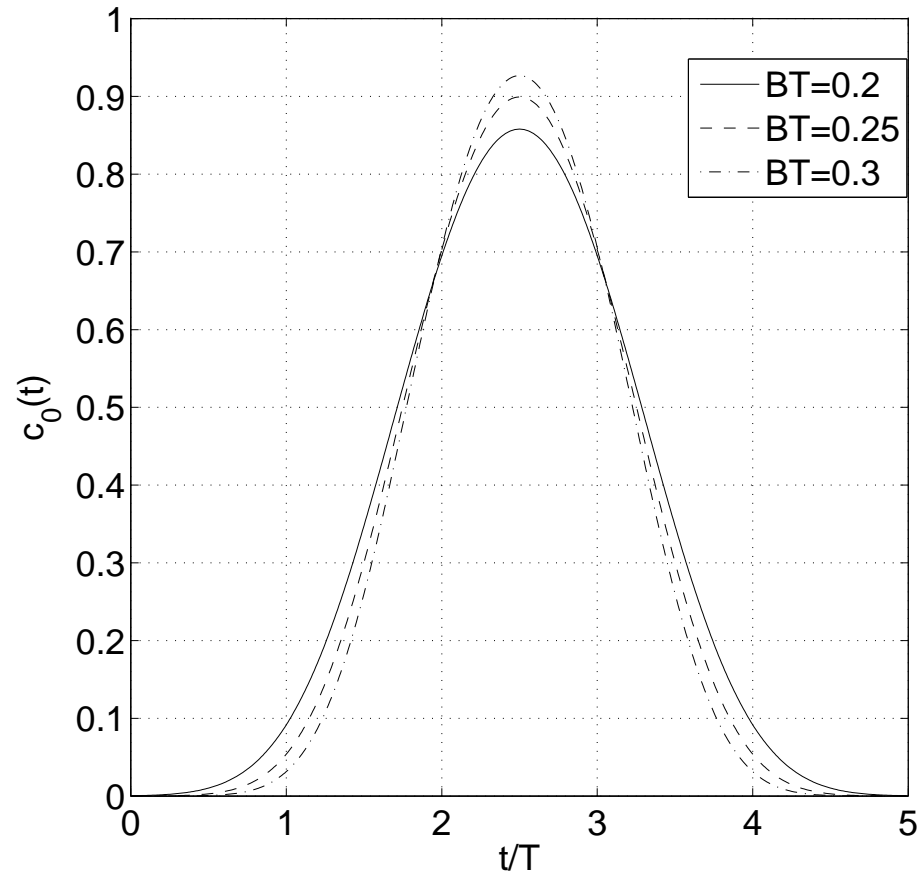
$$c_0(t) = \prod_{n=0}^3 c(t + nT),$$

$$\alpha_{n,0} = \sum_{m=0}^n x_m$$

- Since the GMSK phase shaping pulse is non-causal, when evaluating  $c(t)$  we use the truncated and time shifted GMSK phase shaping pulse

$$\hat{\beta}(t) = \beta(t - 2T)$$

with  $L = 4$  as shown previously.



*LGMSK amplitude shaping pulse for various normalized premodulation filter bandwidths  $BT$ .*

# Linearized Gaussian Minimum Shift Keying (LGMSK)

- For  $h = 1/2$  used in GMSK,

$$a_{n,0} = e^{j\frac{\pi}{2}\alpha_{n,0}} \in \{\pm 1, \pm j\} ,$$

and it follows that

$$\tilde{s}(t) = A \sum_n \left( \hat{x}_{2n+1} c_0(t - 2nT - T) + j \hat{x}_{2n} c_0(t - 2nT) \right)$$

where

$$\begin{aligned} \hat{x}_{2n} &= \hat{x}_{2n-1} x_{2n} \\ \hat{x}_{2n+1} &= -\hat{x}_{2n} x_{2n+1} \\ \hat{x}_{-1} &= 1 \end{aligned}$$

- This is the same as the OQPSK representation for MSK except that the half-sinusoid amplitude pulse shaping function is replaced with the LGMSK amplitude pulse shaping function.
- Note that the LGMSK pulse has length of approximately  $3T$  to  $4T$ , while the pulses on the quadrature branches are transmitted every  $2T$  seconds. Therefore, the LGMSK pulse introduces ISI, but this can be corrected with an equalizer in the receiver.

# POWER SPECTRUM OF BANDPASS SIGNALS

- A bandpass modulated signal can be written in the form

$$\begin{aligned} s(t) &= \Re \left\{ \tilde{s}(t) e^{j(2\pi f_c t)} \right\} \\ &= \frac{1}{2} \left\{ \tilde{s}(t) e^{j(2\pi f_c t)} + \tilde{s}^*(t) e^{-j(2\pi f_c t)} \right\} \end{aligned}$$

- The autocorrelation of a bandpass modulated signal is

$$\begin{aligned} \phi_{ss}(\tau) &= \mathbb{E} [s(t)s(t + \tau)] \\ &= \frac{1}{4} \mathbb{E} \left[ \left( \tilde{s}(t) e^{j2\pi f_c t} + \tilde{s}^*(t) e^{-j2\pi f_c t} \right) \right. \\ &\quad \left. \times \left( \tilde{s}(t + \tau) e^{j(2\pi f_c t + 2\pi f_c \tau)} + \tilde{s}^*(t + \tau) e^{-j(2\pi f_c t + 2\pi f_c \tau)} \right) \right] \\ &= \frac{1}{4} \mathbb{E} \left[ \tilde{s}(t) \tilde{s}(t + \tau) e^{j(4\pi f_c t + 2\pi f_c \tau)} + \tilde{s}(t) \tilde{s}^*(t + \tau) e^{-j2\pi f_c \tau} \right. \\ &\quad \left. + \tilde{s}^*(t) \tilde{s}(t + \tau) e^{j2\pi f_c \tau} + \tilde{s}^*(t) \tilde{s}^*(t + \tau) e^{-j(4\pi f_c t + 2\pi f_c \tau)} \right] \\ &= \frac{1}{4} \left[ \mathbb{E}[\tilde{s}(t) \tilde{s}(t + \tau)] e^{j(4\pi f_c t + 2\pi f_c \tau)} + \mathbb{E}[\tilde{s}(t) \tilde{s}^*(t + \tau)] e^{-j2\pi f_c \tau} \right. \\ &\quad \left. + \mathbb{E}[\tilde{s}^*(t) \tilde{s}(t + \tau)] e^{j2\pi f_c \tau} + \mathbb{E}[\tilde{s}^*(t) \tilde{s}^*(t + \tau)] e^{-j(4\pi f_c t + 2\pi f_c \tau)} \right] . \end{aligned}$$

- If  $s(t)$  is a wide-sense stationary random process, then the exponential terms that involve  $t$  must vanish, i.e.,  $E[\tilde{s}(t)\tilde{s}(t + \tau)] = 0$  and  $E[\tilde{s}^*(t)\tilde{s}^*(t + \tau)] = 0$ .
- Substituting  $\tilde{s}(t) = \tilde{s}_I(t) + j\tilde{s}_Q(t)$  into the above expectations gives the result

$$\begin{aligned}\phi_{\tilde{s}_I\tilde{s}_I}(\tau) &= E[\tilde{s}_I(t)\tilde{s}_I(t + \tau)] = E[\tilde{s}_Q(t)\tilde{s}_Q(t + \tau)] = \phi_{\tilde{s}_Q\tilde{s}_Q}(\tau) \\ \phi_{\tilde{s}_I\tilde{s}_Q}(\tau) &= E[\tilde{s}_I(t)\tilde{s}_Q(t + \tau)] = -E[\tilde{s}_Q(t)\tilde{s}_I(t + \tau)] = -\phi_{\tilde{s}_Q\tilde{s}_I}(\tau)\end{aligned}$$

- Using these results, the autocorrelation is

$$\phi_{ss}(\tau) = \frac{1}{2}\phi_{\tilde{s}\tilde{s}}(\tau)e^{j2\pi f_c\tau} + \frac{1}{2}\phi_{\tilde{s}\tilde{s}}^*(\tau)e^{-j2\pi f_c\tau}$$

where

$$\phi_{\tilde{s}\tilde{s}}(\tau) = \frac{1}{2}E[\tilde{s}^*(t)\tilde{s}(t + \tau)]$$

- The power density spectrum is the Fourier transform of  $\phi_{ss}(\tau)$ :

$$S_{ss}(f) = \frac{1}{2}[S_{\tilde{s}\tilde{s}}(f - f_c) + S_{\tilde{s}\tilde{s}}^*(-f - f_c)]$$

- $S_{\tilde{s}\tilde{s}}(f)$  is the power density spectrum of the complex envelope  $\tilde{s}(t)$ , which is always real-valued but not necessarily even about  $f = 0$ .

$$S_{ss}(f) = \frac{1}{2}[S_{\tilde{s}\tilde{s}}(f - f_c) + S_{\tilde{s}\tilde{s}}(-f - f_c)]$$



# POWER SPECTRAL DENSITY OF A COMPLEX ENVELOPE

- In general, the complex lowpass signal is of the form

$$\tilde{s}(t) = A \sum_k b(t - kT, \mathbf{x}_k)$$

- The autocorrelation of  $\tilde{s}(t)$  is

$$\begin{aligned} \phi_{\tilde{s}\tilde{s}}(t, t + \tau) &= \frac{1}{2} \mathbb{E} [\tilde{s}^*(t) \tilde{s}(t + \tau)] \\ &= \frac{A^2}{2} \sum_i \sum_k \mathbb{E} [b^*(t - iT, \mathbf{x}_i) b(t + \tau - kT, \mathbf{x}_k)] . \end{aligned}$$

Observe that  $\tilde{s}(t)$  is a cyclostationary random process, meaning that the autocorrelation function  $\phi_{\tilde{s}\tilde{s}}(t, t + \tau)$  is periodic in  $t$  with period  $T$ . To see this property, first note that

$$\begin{aligned} \phi_{\tilde{s}\tilde{s}}(t + T, t + T + \tau) &= \frac{A^2}{2} \sum_i \sum_k \mathbb{E} [b^*(t + T - iT, \mathbf{x}_i) b(t + T + \tau - kT, \mathbf{x}_k)] \\ &= \frac{A^2}{2} \sum_{i'} \sum_{k'} \mathbb{E} [b^*(t - i'T, \mathbf{x}_{i'+1}) b(t + \tau - k'T, \mathbf{x}_{k'+1})] . \end{aligned}$$

- Under the assumption that the information sequence is a stationary random process it follows that

$$\begin{aligned}
\phi_{\tilde{s}\tilde{s}}(t + T, t + T + \tau) &= \frac{A^2}{2} \sum_{i'} \sum_{k'} \mathbb{E} [b^*(t - i'T, \mathbf{x}_{i'}) b(t + \tau - k'T, \mathbf{x}_{k'})] \\
&= \phi_{\tilde{s}\tilde{s}}(t, t + \tau) .
\end{aligned} \tag{5}$$

where data blocks  $\mathbf{x}_{i'+1}$  and  $\mathbf{x}_{k'+1}$  are replaced by  $\mathbf{x}_{i'}$  and  $\mathbf{x}_{k'}$ , respectively. Therefore  $\tilde{s}(t)$  is cyclostationary.

- Since  $\tilde{s}(t)$  is cyclostationary, the autocorrelation  $\phi_{\tilde{s}\tilde{s}}(\tau)$  can be obtained by taking the time average of  $\phi_{\tilde{s}\tilde{s}}(t, t + \tau)$ , given by

$$\begin{aligned}
\phi_{\tilde{s}\tilde{s}}(\tau) &= \langle \phi_{\tilde{s}\tilde{s}}(t, t + \tau) \rangle \\
&= \frac{A^2}{2} \sum_i \sum_k \frac{1}{T} \int_0^T \mathbb{E} [b^*(t - iT, \mathbf{x}_i) b(t + \tau - kT, \mathbf{x}_k)] dt \\
&= \frac{A^2}{2T} \sum_i \sum_k \int_{-iT}^{-iT+T} \mathbb{E} [b^*(z, \mathbf{x}_i) b(z + \tau - (k - i)T, \mathbf{x}_k)] dz \\
&= \frac{A^2}{2T} \sum_i \sum_m \int_{-iT}^{-iT+T} \mathbb{E} [b^*(z, \mathbf{x}_i) b(z + \tau - mT, \mathbf{x}_{m+i})] dz \\
&= \frac{A^2}{2T} \sum_i \sum_m \int_{-iT}^{-iT+T} \mathbb{E} [b^*(z, \mathbf{x}_0) b(z + \tau - mT, \mathbf{x}_m)] dz \\
&= \frac{A^2}{2T} \sum_m \int_{-\infty}^{\infty} \mathbb{E} [b^*(z, \mathbf{x}_0) b(z + \tau - mT, \mathbf{x}_m)] dz ,
\end{aligned}$$

where  $\langle \cdot \rangle$  denotes time averaging and the second last equality used the stationary property of the data sequence  $\{\mathbf{x}_k\}$ .

- The psd of  $\tilde{s}(t)$  is obtained by taking the Fourier transform of  $\phi_{\tilde{s}\tilde{s}}(\tau)$ ,

$$\begin{aligned}
S_{\tilde{s}\tilde{s}}(f) &= \mathbb{E} \left[ \frac{A^2}{2T} \sum_m \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} b^*(z, \mathbf{x}_0) b(z + \tau - mT, \mathbf{x}_m) dz e^{-j2\pi f\tau} d\tau \right] \\
&= \mathbb{E} \left[ \frac{A^2}{2T} \sum_m \int_{-\infty}^{\infty} b^*(z, \mathbf{x}_0) e^{j2\pi fz} dz \right. \\
&\quad \left. \times \int_{-\infty}^{\infty} b(z + \tau - mT, \mathbf{x}_m) e^{-j2\pi f(z+\tau-mT)} d\tau e^{-j2\pi fmT} \right] \\
&= \mathbb{E} \left[ \frac{A^2}{2T} \sum_m \int_{-\infty}^{\infty} b^*(z, \mathbf{x}_0) e^{-j2\pi fz} dz \int_{-\infty}^{\infty} b(\tau', \mathbf{x}_m) e^{-j2\pi f\tau'} d\tau' e^{-j2\pi fmT} \right] \\
&= \frac{A^2}{2T} \sum_m \mathbb{E} [B^*(f, \mathbf{x}_0) B(f, \mathbf{x}_m)] e^{-j2\pi fmT},
\end{aligned}$$

where  $B(f, \mathbf{x}_m)$  is the Fourier transform of  $b(t, \mathbf{x}_m)$ .

- Finally,

$$S_{\tilde{s}\tilde{s}}(f) = \frac{A^2}{T} \sum_m S_{b,m}(f) e^{-j2\pi fmT}$$

where

$$S_{b,m}(f) = \frac{1}{2} \mathbb{E} [B^*(f, \mathbf{x}_0) B(f, \mathbf{x}_m)]$$

- Suppose that  $\mathbf{x}_m$  and  $\mathbf{x}_0$  are uncorrelated for  $|m| \geq K$ .
- Then

$$S_{b,m}(f) = S_{b,K}(f), \quad |m| \geq K$$

where

$$\begin{aligned} S_{b,K}(f) &= \frac{1}{2} \mathbb{E} [B^*(f, \mathbf{x}_0)] \mathbb{E} [B(f, \mathbf{x}_m)] \quad |m| \geq K \\ &= \frac{1}{2} \mathbb{E} [B^*(f, \mathbf{x}_0)] \mathbb{E} [B(f, \mathbf{x}_0)] \quad |m| \geq K \\ &= \frac{1}{2} |\mathbb{E} [B(f, \mathbf{x}_0)]|^2, \quad |m| \geq K. \end{aligned}$$

- It follows that

$$S_{\tilde{s}\tilde{s}}(f) = S_{\tilde{s}\tilde{s}}^c(f) + S_{\tilde{s}\tilde{s}}^d(f)$$

where

$$\begin{aligned} S_{\tilde{s}\tilde{s}}^c(f) &= \frac{A^2}{T} \sum_{|m| < K} (S_{b,m}(f) - S_{b,K}(f)) e^{-j2\pi f m T} \\ S_{\tilde{s}\tilde{s}}^d(f) &= \left(\frac{A}{T}\right)^2 S_{b,K}(f) \sum_n \delta\left(f - \frac{n}{T}\right) \end{aligned}$$

- Note that the spectrum consists of discrete and continuous parts. The discrete portion has spectral lines spaced at  $1/T$  Hz apart.

# ZERO MEAN SIGNALS

- If  $\tilde{s}(t)$  has zero mean, i.e.,  $\mathbb{E}[b(t, \mathbf{x}_0)] = 0$ , then  $\mathbb{E}[B(f, \mathbf{x}_0)] = 0$ .
- Under this condition

$$S_{b,K}(f) = \frac{1}{2} |\mathbb{E}[B(f, \mathbf{x}_0)]|^2 = 0$$

- Hence,  $S_{\tilde{s}\tilde{s}}(f)$  has no discrete component and

$$S_{\tilde{s}\tilde{s}}(f) = \left(\frac{A^2}{T}\right) \sum_{|m| < K} S_{b,m}(f) e^{-j2\pi f m T}$$

# UNCORRELATED SOURCE SYMBOLS

- With uncorrelated source symbols the information symbols  $x_{m,k}$  constituting data blocks  $\mathbf{x}_m = (x_{m,1}, x_{m,2}, \dots, x_{m,N})$  are mutually uncorrelated. Under this condition  $\mathbf{x}_m$  and  $\mathbf{x}_0$  are obviously uncorrelated for  $|m| \geq 1$ .
- Hence,  $S_{b,m}(f) = S_{b,1}(f)$ , for  $|m| \geq 1$ , where

$$S_{b,0}(f) = \frac{1}{2} \text{E} [ |B(f, \mathbf{x}_0)|^2 ]$$

$$S_{b,1}(f) = \frac{1}{2} | \text{E} [ B(f, \mathbf{x}_0) ] |^2$$

- Hence

$$S_{\tilde{s}\tilde{s}}^d(f) = \frac{A^2}{T^2} S_{b,1}(f) \sum_n \delta(f - n/T)$$

$$S_{\tilde{s}\tilde{s}}^c(f) = \frac{A^2}{T} (S_{b,0}(f) - S_{b,1}(f))$$

- If  $\tilde{s}(t)$  has zero mean as well, then

$$S_{\tilde{s}\tilde{s}}(f) = \frac{A^2}{T} S_{b,0}(f)$$

# LINEAR FULL RESPONSE MODULATION

- Here it is assumed that

$$\begin{aligned}b(t, \mathbf{x}_k) &= x_k h_a(t) \\ B(f, \mathbf{x}_k) &= x_k H_a(f) ,\end{aligned}$$

where the  $x_k$  may be correlated.

- Using the above leads to

$$\begin{aligned}S_{b,m}(f) &= \frac{1}{2} \mathbb{E} [B^*(f, \mathbf{x}_0) B(f, \mathbf{x}_m)] \\ &= \frac{1}{2} \mathbb{E} [x_0^* H_a^*(f) x_m H_a(f)] \\ &= \frac{1}{2} \mathbb{E} [x_0^* x_m |H_a(f)|^2] \\ &= \frac{1}{2} \mathbb{E} [x_0^* x_m] |H_a(f)|^2 \\ &= \phi_{xx}(m) |H_a(f)|^2\end{aligned}$$

where

$$\phi_{xx}(m) = \frac{1}{2} \mathbb{E} [x_k^* x_{k+m}]$$



- The psd of the complex envelope is

$$\begin{aligned}
S_{\tilde{s}\tilde{s}}(f) &= \frac{A^2}{T} \sum_m S_{b,m}(f) e^{-j2\pi f m T} \\
&= \frac{A^2}{T} |H_a(f)|^2 \sum_m \phi_{xx}(m) e^{-j2\pi f m T} \\
&= \frac{A^2}{T} |H_a(f)|^2 S_{xx}(f)
\end{aligned}$$

where

$$S_{xx}(f) = \sum_m \phi_{xx}(m) e^{-j2\pi f m T}$$

- With uncorrelated source symbols

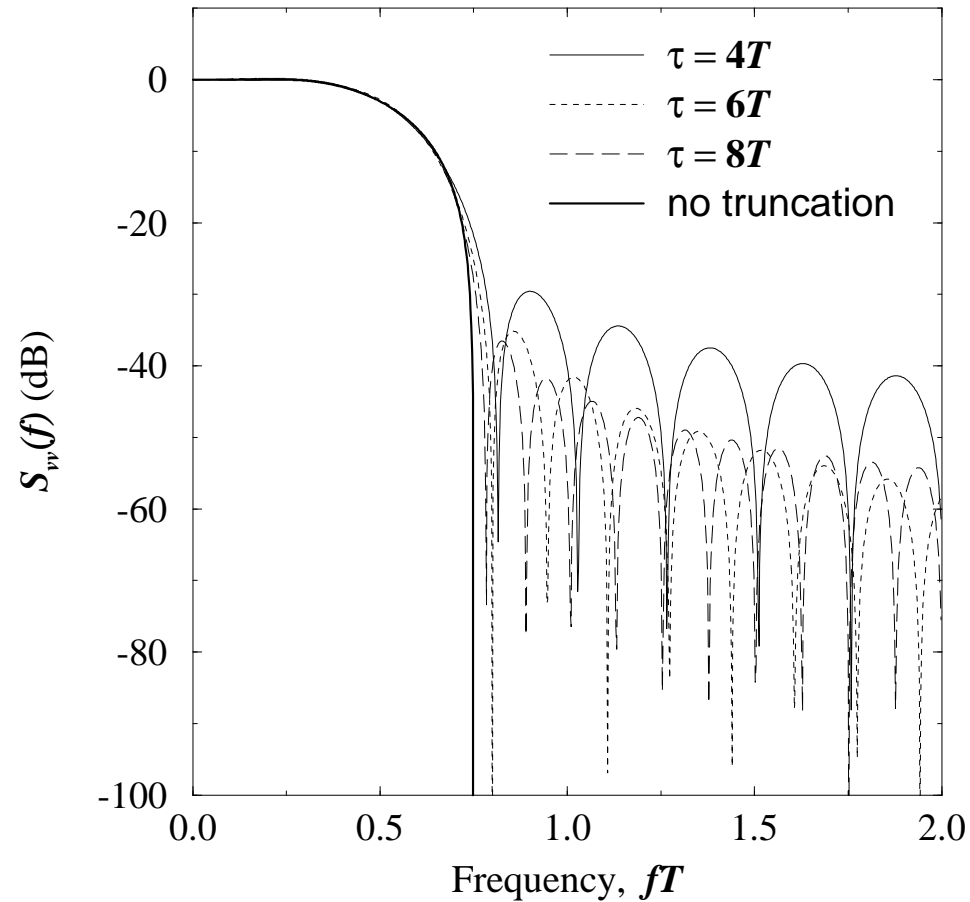
$$\begin{aligned}
S_{b,0}(f) &= \sigma_x^2 |H_a(f)|^2 \\
S_{b,m}(f) &= \frac{1}{2} |\mu_x|^2 |H_a(f)|^2, \quad |m| \geq 1.
\end{aligned}$$

where  $\sigma_x^2 = \frac{1}{2} \mathbb{E}[|x_k|^2]$ ,  $\mu_x = \mathbb{E}[x_k]$ .

- If  $\mu_x = 0$ , then  $S_{b,1}(f) = 0$  and

$$S_{\tilde{s}\tilde{s}}(f) = \frac{A^2}{T} \sigma_x^2 |H_a(f)|^2$$

# POWER SPECTRAL DENSITY OF ASK



*Psd of ASK with a truncated square root raised cosine pulse with various truncation lengths;  $\beta = 0.5$ .*

# OFDM Power Spectrum

- The data symbols  $x_{n,k}$ ,  $k = 0, \dots, N - 1$  that modulate the  $N$  sub-carriers are assumed to have zero mean, variance  $\sigma_x^2 = \frac{1}{2}\mathbb{E}[|x_{n,k}|^2]$ , and they are mutually uncorrelated.
- In this case, the psd of the OFDM waveform is

$$S_{\tilde{s}\tilde{s}}(f) = \frac{A^2}{T_g} S_{b,0}(f) \ ,$$

where

$$S_{b,0}(f) = \frac{1}{2}\mathbb{E} \left[ |B(f, \mathbf{x}_0)|^2 \right] \ ,$$

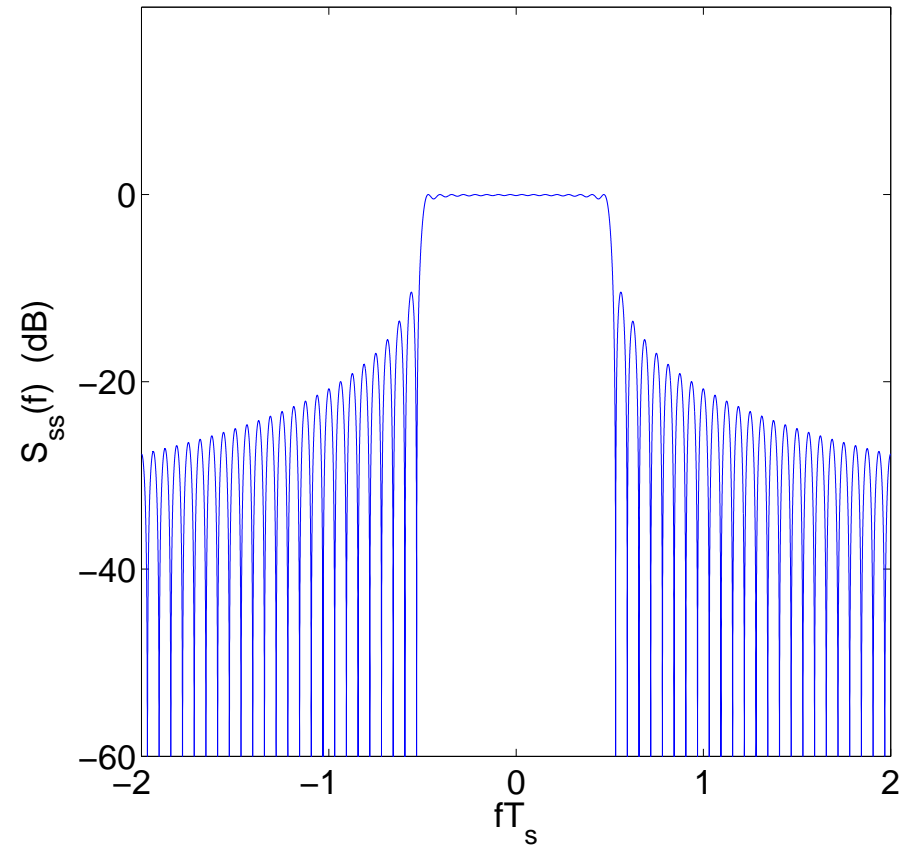
and

$$B(f, \mathbf{x}_0) = \sum_{k=0}^{N-1} x_{0,k} T \text{sinc}(fT - k) + \sum_{k=0}^{N-1} x_{0,k} \alpha_g T \text{sinc}(\alpha_g(fT - k)) e^{j2\pi fT} \ .$$

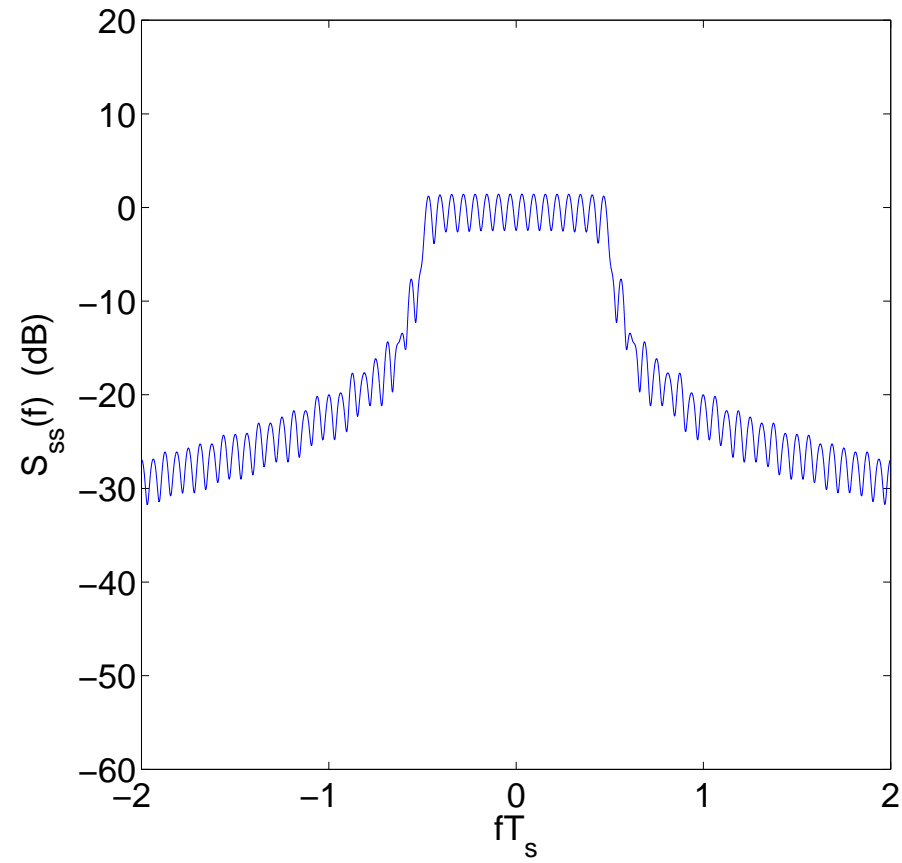
Using the above along with  $T = NT_s$  yields the result

$$\begin{aligned} S_{\tilde{s}\tilde{s}}(f) = & \sigma_x^2 A^2 T \left( \frac{1}{1 + \alpha_g} \sum_{k=0}^{N-1} \text{sinc}^2(NfT_s - k) \right. \\ & + \frac{\alpha_g^2}{1 + \alpha_g} \sum_{k=0}^{N-1} \text{sinc}^2(\alpha_g(NfT_s - k)) \\ & \left. + \frac{2\alpha_g}{1 + \alpha_g} \cos(2\pi NfT_s) \sum_{k=0}^{N-1} \text{sinc}(NfT_s - k) \text{sinc}(\alpha_g(NfT_s - k)) \right) \ . \end{aligned}$$

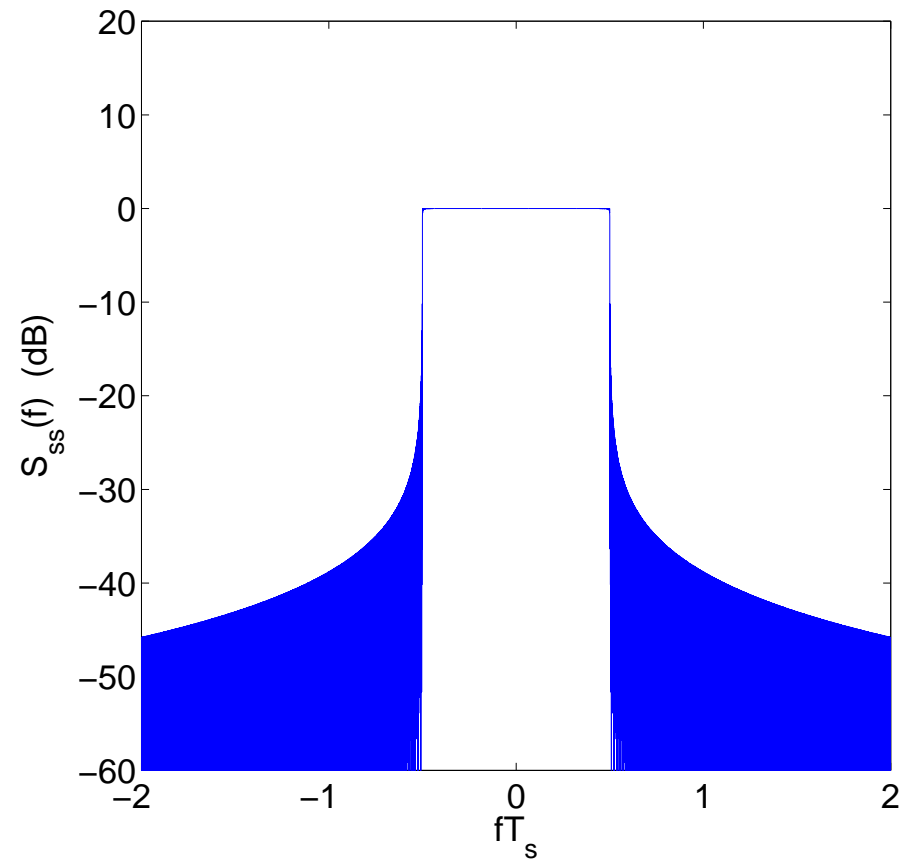
- Note that the Nyquist frequency in this case is  $1/2T_s^g = (1 + \alpha_g)/2T_s$ .



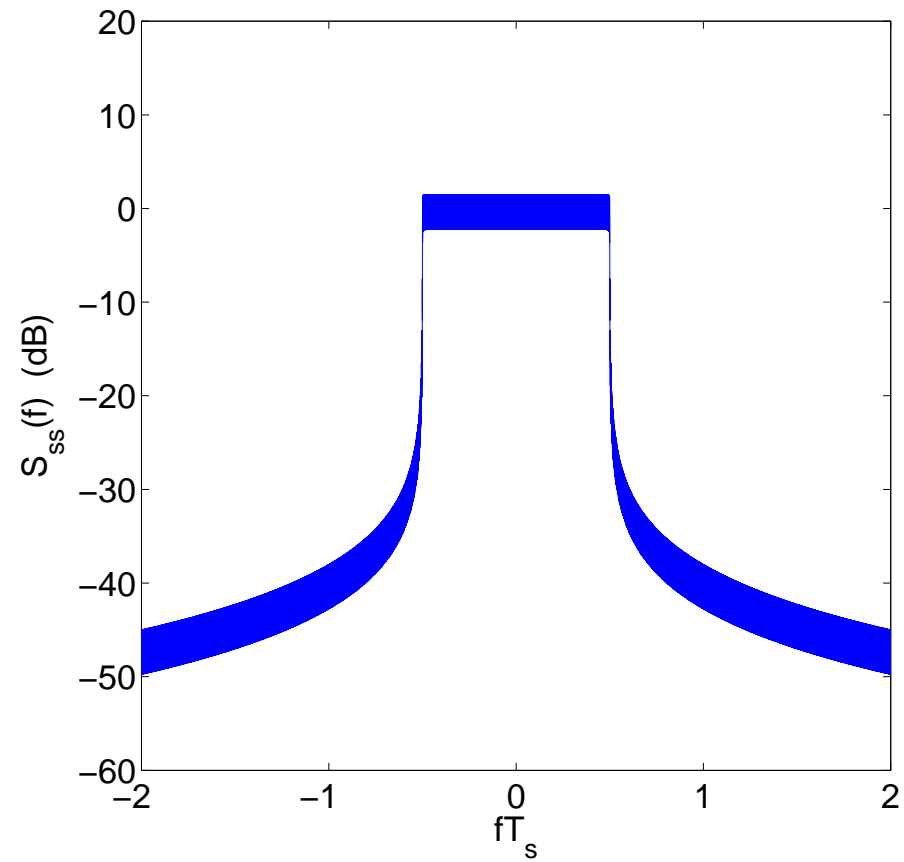
*Psd of OFDM with  $N = 16, \alpha_g = 0$ .*



*Psd of OFDM with  $N = 16, \alpha_g = 0.25$ .*



*Psd of OFDM with  $N = 1024, \alpha_g = 0$ .*



*Psd of OFDM with  $N = 1024, \alpha_g = 0.25$ .*

# OFDM Power Spectrum -IFFT Implementation

- The output of the IDFT baseband modulator is  $\{\mathbf{X}^g\} = \{X_{n,m}^g\}$ , where  $m$  is the block index and

$$\begin{aligned} X_{n,m}^g &= X_{n,(m)_N} \\ &= A \sum_{k=0}^{N-1} x_{n,k} e^{\frac{j2\pi km}{N}}, \quad m = 0, 1, \dots, N + G - 1 \end{aligned}$$

- The power spectrum of the sequence  $\{\mathbf{X}^g\}$  can be calculated by first determining the discrete-time autocorrelation function of the time-domain sequence  $\{\mathbf{X}^g\}$  and then taking a discrete-time Fourier transform of the discrete-time autocorrelation function.
- The psd of the OFDM complex envelope with ideal DACs can be obtained by applying the resulting power spectrum to an ideal low-pass filter with a cutoff frequency of  $1/(2T_s^g)$  Hz.



# Discrete-time Autocorrelation Function

- The time-domain sequence  $\{\mathbf{X}^g\}$  is a periodic wide-sense stationary sequence having the discrete-time autocorrelation function

$$\begin{aligned}\phi_{X^g X^g}(m, \ell) &= \frac{1}{2} \mathbb{E}[(X_{n,m}^g)^* X_{n,m+\ell}^g] \\ &= A^2 \sum_{k=0}^{N-1} \sum_{i=0}^{N-1} \frac{1}{2} \mathbb{E}[x_{n,k}^* x_{n,i}] e^{j \frac{2\pi}{N} (-km + im + i\ell)}, \\ &\quad \text{for } m = 0, \dots, N + G - 1 .\end{aligned}$$

The data symbols,  $x_{n,k}$ , are assumed to be mutually uncorrelated with zero mean and variance  $\sigma_x^2 = \frac{1}{2} \mathbb{E}[|x_{n,k}|^2]$ . Using the fact, that  $X_{n,m}^g = X_{n,(m)_N}$ , it follows that

$$\phi_{X^g X^g}(m, \ell) = \begin{cases} A\sigma_x^2 & m = 0, \dots, G - 1, \ell = 0, N \\ & m = G, \dots, N - 1, \ell = 0 \\ & m = N, \dots, N + G - 1, \ell = 0, -N \\ 0 & \text{otherwise} \end{cases} .$$

Averaging over all time indices  $m$  in a block gives the time-average discrete-time autocorrelation function

$$\phi_{X^g X^g}(\ell) = \begin{cases} A\sigma_x^2 & \ell = 0 \\ \frac{G}{N+G} A\sigma_x^2 & \ell = -N, N \\ 0 & \text{otherwise} \end{cases} .$$

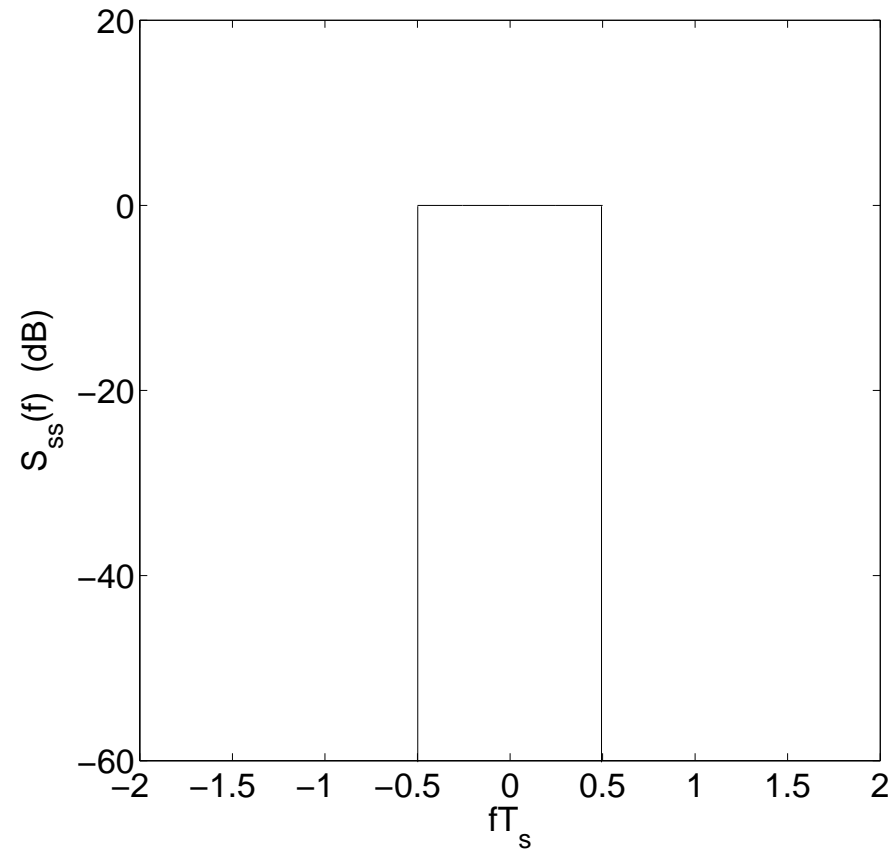
# Power Spectrum

- Taking the discrete-time Fourier transform of the discrete-time autocorrelation function gives

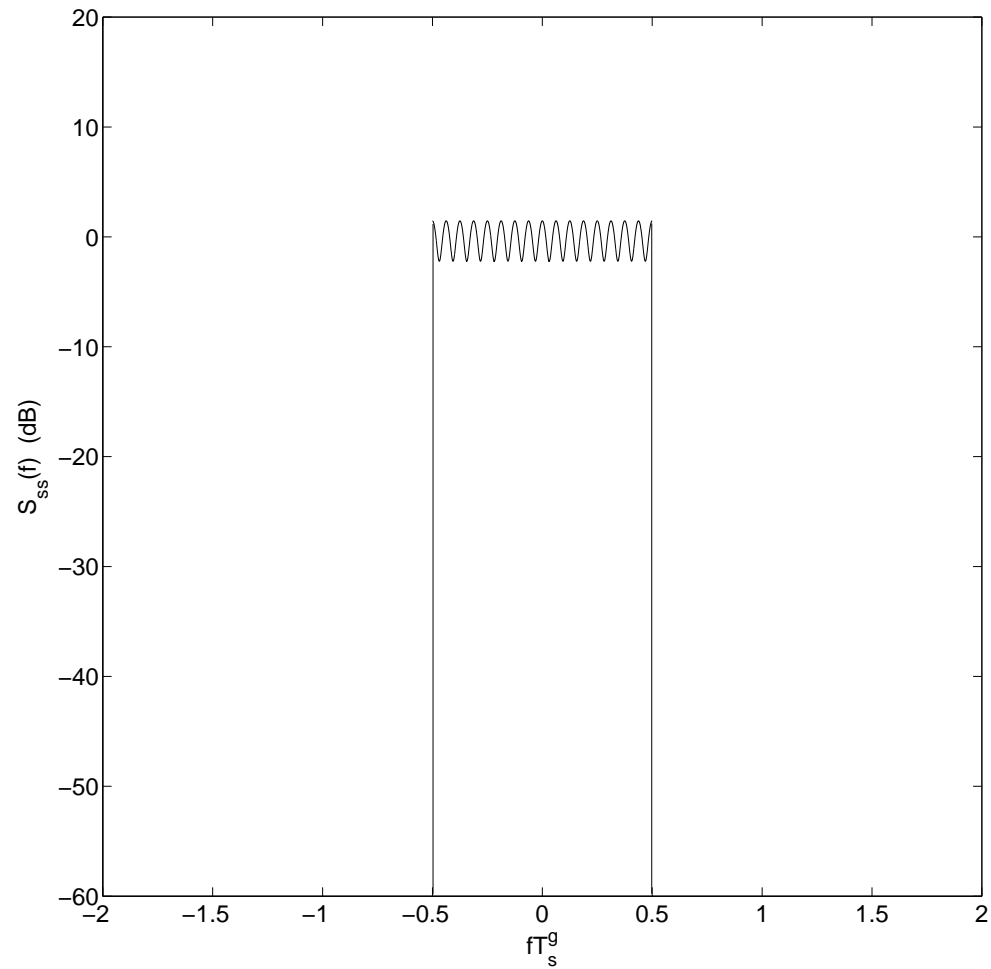
$$\begin{aligned}
 S_{X^g X^g}(f) &= \sum_m \phi_{X^g X^g}(\ell) e^{-j2\pi f m N T_s^g} \\
 &= A\sigma_x^2 \left( 1 + \frac{G}{N+G} e^{-j2\pi f N T_s^g} + \frac{G}{N+G} e^{j2\pi f N T_s^g} \right) \\
 &= A\sigma_x^2 \left( 1 + \frac{2G}{N+G} \cos(2\pi f N T_s^g) \right) .
 \end{aligned}$$

- Finally, assume that the sequence  $\{\mathbf{X}^g\} = \{X_{n,m}^g\}$  is passed through an ideal DACs.
  - The ideal DAC is a low-pass filter with cutoff frequency  $1/(2T_s^g)$ .
- The OFDM complex envelope has the psd

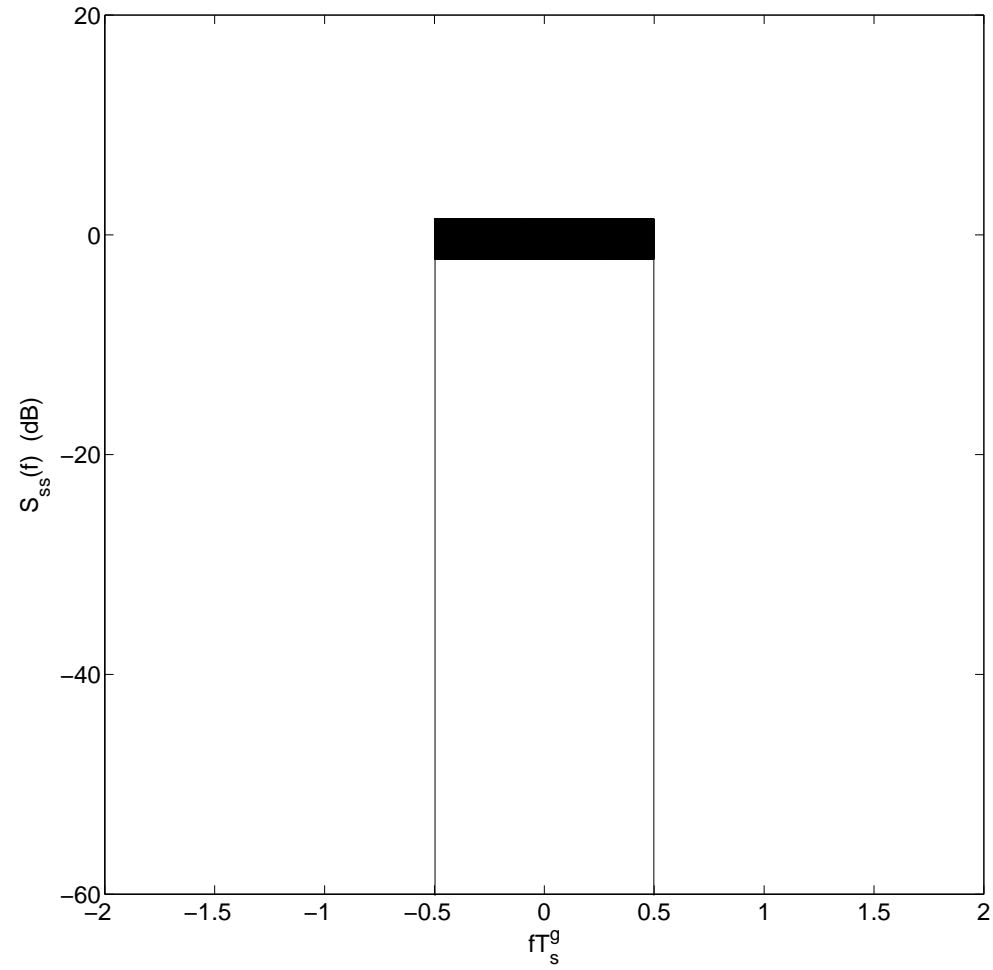
$$S_{\tilde{s}\tilde{s}}(f) = A\sigma_x^2 \left( 1 + \frac{2G}{N+G} \cos(2\pi f N T_s^g) \right) \text{rect}(f T_s^g) .$$



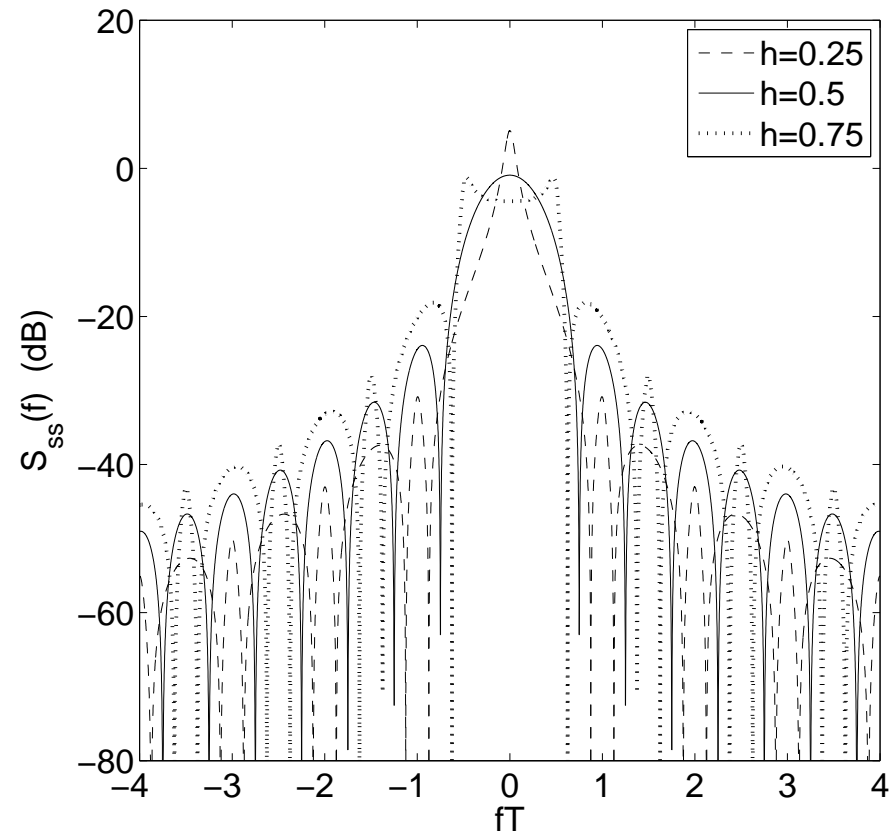
*Psd of IDFT-based OFDM with  $N = 16, G = 0$ . Note in this case that  $T_s^g = T_s$ .*



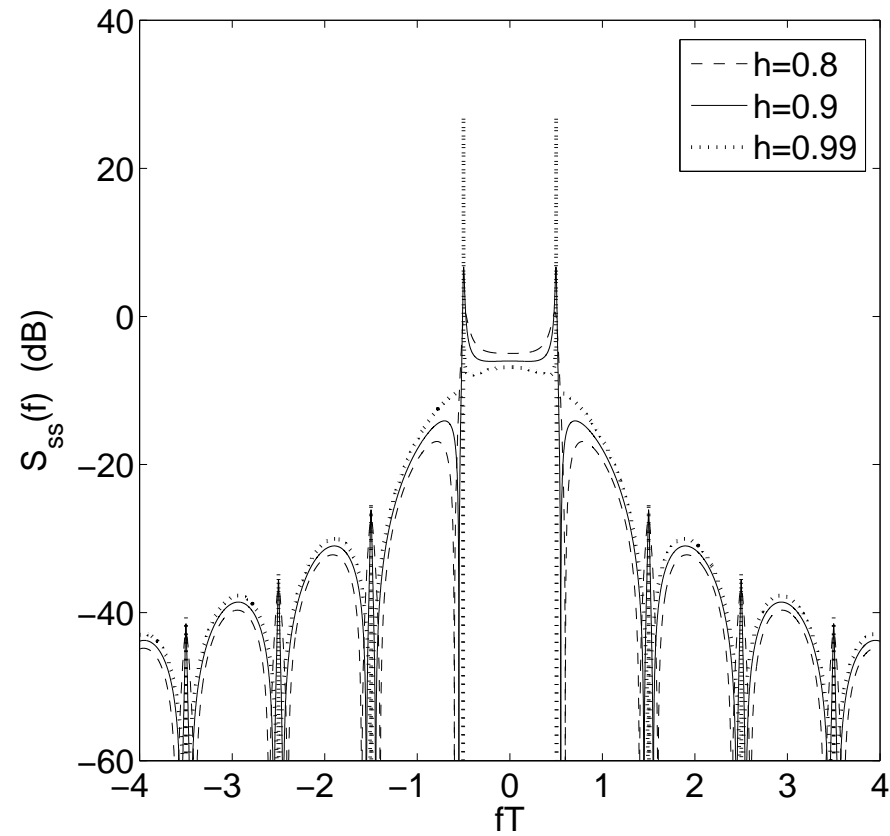
*Psd of IDFT-based OFDM with  $N = 16, G = 4$ .*



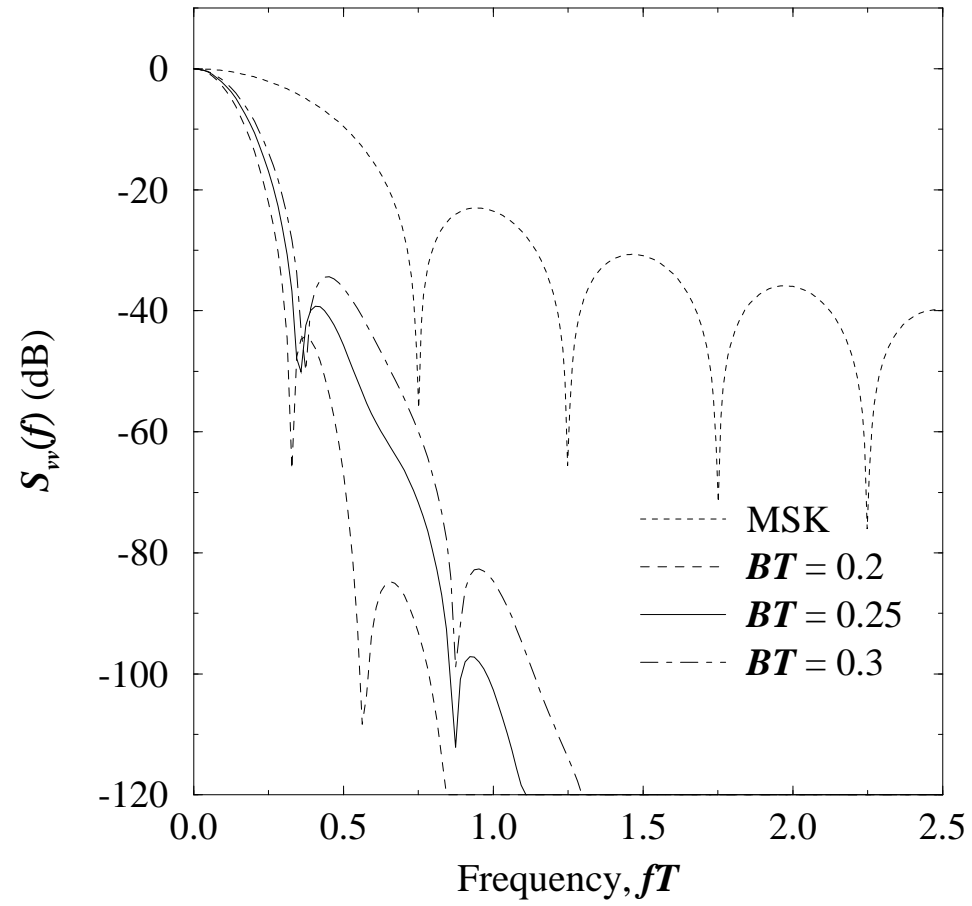
*Psd of IDFT-based OFDM with  $N = 1024, G = 256$ .*



*Power spectral density of binary CPFSK for various modulation indices.*



*PsD of binary CPFSK as the modulation index  $h \rightarrow 1$ .*



*Power spectral density of GMSK with various normalized filter bandwidths  $BT$ .*