

ECE 6604 Assignment #7 Solutions

✓ 6.7 a) DPSK $P_b(\gamma_b) = \frac{1}{2} e^{-\gamma_b}$; $\gamma_b = \alpha^2 \frac{E_b}{N_0}$

$$\bar{P}_b = \int_0^\infty P_b(x) p_{\gamma_b}(x) dx$$

But $p_{\gamma_b}(x) = 0.2 \delta(x) + 0.5 \delta(x - E_b/N_0) + 0.3 \delta(x - 4E_b/N_0)$

$$P_b = 0.1 + 0.25 e^{-E_b/N_0} + 0.15 e^{-4E_b/N_0}$$

Let $\bar{\gamma}_b = E[\gamma_b] = (0.2)0 + (E_b/N_0)(0.5) + (4E_b/N_0)(0.3) = 1.7 \frac{E_b}{N_0}$

$$\bar{P}_b = 0.1 + 0.25 e^{-\bar{\gamma}_b/1.7} + 0.15 e^{-4\bar{\gamma}_b/1.7}$$

As $\bar{\gamma}_b \rightarrow \infty$, $\bar{P}_b \rightarrow 0.1$

b) $\gamma_b = \max(\gamma_1, \gamma_2)$; $\gamma_1 = \alpha_1^2 \frac{E_b}{N_0}$, $\gamma_2 = \alpha_2^2 \frac{E_b}{N_0}$

$F_{\gamma_b}(x) = F_{\gamma_1}(x) \cdot F_{\gamma_2}(x) = [F_{\gamma_1}(x)]^2$ since α_1 and α_2 are iid.

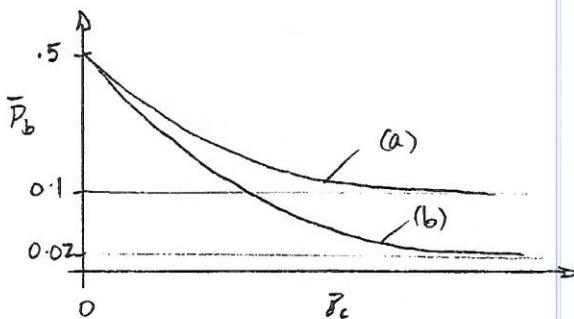
$$P_{\gamma_b}(x) = \frac{d}{dx} F_{\gamma_b}(x) = 0.04 \delta(x) + 0.45 \delta(x - E_b/N_0) + 0.51 \delta(x - 4E_b/N_0)$$

$$\bar{P}_b = 0.02 + 0.225 e^{-E_b/N_0} + 0.255 e^{-4E_b/N_0}$$

$$\bar{\gamma}_c = 1.7 \frac{E_b}{N_0} \text{ as before}$$

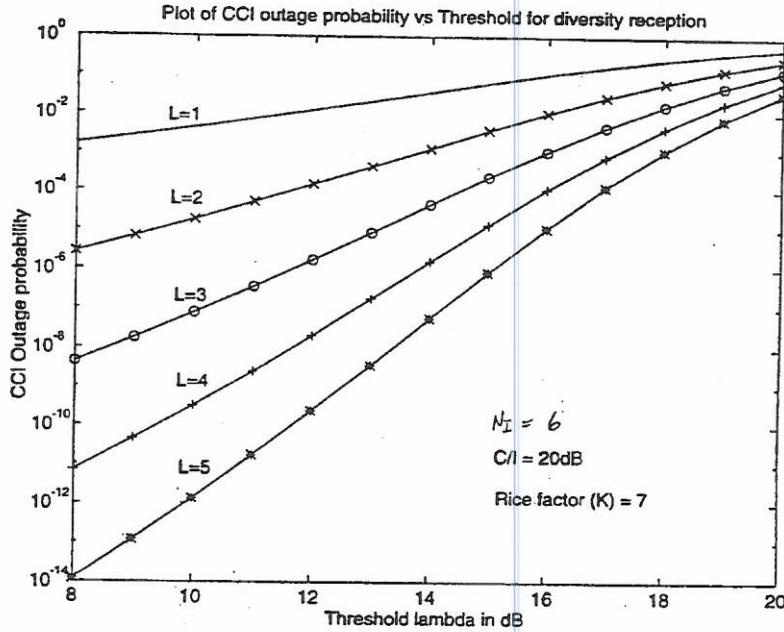
$$\bar{P}_b = 0.02 + 0.225 e^{-\bar{\gamma}_c/1.7} + 0.255 e^{-4\bar{\gamma}_c/1.7}$$

As $\bar{\gamma}_c \rightarrow \infty$, $\bar{P}_b \rightarrow 0.02$



For case (a) $\bar{P}_b = \bar{P}_c$

2/ 6.14 $O = \Pr(\lambda_s < \lambda_{th}) = \Pr(\lambda_1 < \lambda_{th}, \lambda_2 < \lambda_{th}, \dots, \lambda_L < \lambda_{th}) = [\Pr(\lambda_1 < \lambda_{th})]^L$, (since λ_i 's are i.i.d.)
 where $\Pr(\lambda_1 < \lambda_{th}) = \frac{\lambda_{th}}{\lambda_{th} + b_1} e^{-\frac{Kb_1}{\lambda_{th} + b_1}} \left\{ \sum_{k=0}^{N_I-1} \left(\frac{b_1}{\lambda_{th} + b_1} \right)^k \sum_{m=0}^k \binom{k}{m} \frac{1}{m!} \left(\frac{K\lambda_{th}}{\lambda_{th} + b_1} \right)^m \right\}$
 $b_1 = \frac{\Omega_o}{(K+1)\Omega_1} = \frac{N_I \Delta}{(K+1)} , \Delta \cong CIR = \frac{\Omega_o}{N_I \Omega_1}$ < see Problem *3.7 for derivation >



3/ 6.15 a) We will find the cdf of λ as follows:

$$\begin{aligned}
 F_\lambda(x) &= P(\lambda = \frac{s_0}{s_1} \leq x) = \int_0^\infty \int_0^{xs_1} p_{s_0}(s_0) p_{s_1}(s_1) ds_0 ds_1 \\
 &= \int_0^\infty \int_0^{xs_1} \frac{1}{s_0} e^{-s_0/\bar{s}_0} \frac{1}{s_1} e^{-s_1/\bar{s}_1} ds_0 ds_1 \\
 &= \frac{1}{s_1} \int_0^\infty e^{-s_1/\bar{s}_1} \left\{ -e^{-s_0/\bar{s}_0} \Big|_0^{xs_1} \right\} ds_1 = \frac{1}{s_1} \int_0^\infty e^{-s_1/\bar{s}_1} \left[1 - e^{-xs_1/\bar{s}_0} \right] ds_1 \\
 &= \frac{1}{s_1} \int_0^\infty e^{-s_1/\bar{s}_1} ds_1 - \frac{1}{s_1} \int_0^\infty e^{-s_1 \left(\frac{1}{\bar{s}_1} + \frac{x}{\bar{s}_0} \right)} ds_1 \\
 &= 1 - \frac{1}{1 + \frac{\bar{s}_1}{\bar{s}_0} x} = \frac{x}{\frac{\bar{s}_0}{\bar{s}_1} + x} = \frac{x}{\bar{\lambda} + x}
 \end{aligned}$$

The pdf of λ is just the derivative of its cdf and is

$$p_\lambda(x) = \frac{\bar{\lambda}}{(x + \bar{\lambda})^2} \text{ for } \lambda \geq 0.$$

b) The mean value of λ is

$$\mathbb{E}[\lambda] = \int_0^\infty x p_\lambda(x) dx = \int_0^\infty \frac{x \bar{\lambda}}{(x + \bar{\lambda})^2} dx = \infty.$$

c) When the selection diversity combining is used the output of the selection combiner will be

$$\lambda_b^s = \max\{\lambda_1, \dots, \lambda_L\}$$

The cdf of the signal-to-interference ratio at the output of the selection combiner will be

$$F_{\lambda_b^s}(x) = \left(\frac{x}{x + \bar{\lambda}}\right)^L.$$

The pdf of λ_b^s will be the derivative of its cdf, i.e.

$$p_{\lambda_b^s}(x) = L \left(\frac{x}{x + \bar{\lambda}}\right)^{L-1} \frac{\bar{\lambda}}{(x + \bar{\lambda})^2}$$

16.07

$$\bar{J} = 2\bar{w}^T \bar{\Phi}_{\tilde{S}_t \tilde{R}_t} \bar{w}^* - 2\operatorname{Re}\left\{\bar{\Phi}_{\tilde{S}_0 \tilde{R}_t} \bar{w}^*\right\} - 2E_{av}$$

For the gradient of real-valued \bar{J} wrt complex \bar{w}

$$\nabla_{\bar{w}} \bar{J} = \nabla_{\bar{w}_R} \bar{J} + j \nabla_{\bar{w}_I} \bar{J}$$

$$\bar{\Phi}_{\tilde{S}_t \tilde{R}_t} = \bar{\Phi}_{\tilde{S}_t \tilde{R}_t R} + j \bar{\Phi}_{\tilde{S}_t \tilde{R}_t I}$$

$$\bar{\Phi}_{\tilde{S}_0 \tilde{R}_t} = \bar{\Phi}_{\tilde{S}_0 \tilde{R}_t R} + j \bar{\Phi}_{\tilde{S}_0 \tilde{R}_t I}$$

$$\begin{aligned} \nabla_{\bar{w}_R} \operatorname{Re}\left\{\bar{\Phi}_{\tilde{S}_0 \tilde{R}_t} \bar{w}^*\right\} &= \nabla_{\bar{w}_R} \operatorname{Re}\left\{\left(\bar{\Phi}_{\tilde{S}_0 \tilde{R}_t R} + j \bar{\Phi}_{\tilde{S}_0 \tilde{R}_t I}\right)(\bar{w}_R - j \bar{w}_I)\right\} \\ &= \nabla_{\bar{w}_R} \left\{ \bar{\Phi}_{\tilde{S}_0 \tilde{R}_t R} \bar{w}_R + \bar{\Phi}_{\tilde{S}_0 \tilde{R}_t I} \bar{w}_I \right\} \\ &= \bar{\Phi}_{\tilde{S}_0 \tilde{R}_t R} \end{aligned}$$

likewise,

$$\nabla_{W_I} \operatorname{Re} \left\{ \Phi_{\tilde{\zeta}_0 \tilde{\zeta}_I} W^* \right\} = \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I}$$

$$\begin{aligned} \underline{W}^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}^* &= (\underline{W}_R^T + j \underline{W}_I^T) (\bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_R} + j \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I}) (\underline{W}_R - j \underline{W}_I) \\ &= (\underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_R} - \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} + j (\underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} + \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_R})) \\ &\quad \times (\underline{W}_R - j \underline{W}_I) \\ &= \underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_R} \underline{W}_R - \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}_R + \underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}_I \\ &\quad + \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_R} \underline{W}_I \\ &\quad + j \left\{ \underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}_R + \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_R} \underline{W}_R - \underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}_I \right. \\ &\quad \left. + \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}_I \right\} \end{aligned}$$

but

$$\underline{W}^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}^* \text{ is real}$$

and

$$\begin{aligned} \underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}_I &= (\underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}_I)^T \\ &= \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I}^T \underline{W}_R \\ &= - \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}_R \end{aligned}$$

so

$$\begin{aligned} \underline{W}^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}^* &= \underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_R} \underline{W}_R - \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}_R \\ &\quad + \underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}_I + \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_R} \underline{W}_I \end{aligned}$$

$$\Rightarrow \nabla_{W_R} \underline{W}^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}^* = 2 \underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_R} - 2 \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I}$$

$$\nabla_{W_I} \underline{W}^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I} \underline{W}^* = 2 \underline{W}_I^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_R} + 2 \underline{W}_R^T \bar{\Phi}_{\tilde{\zeta}_0 \tilde{\zeta}_I}$$

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Hence, combining the above

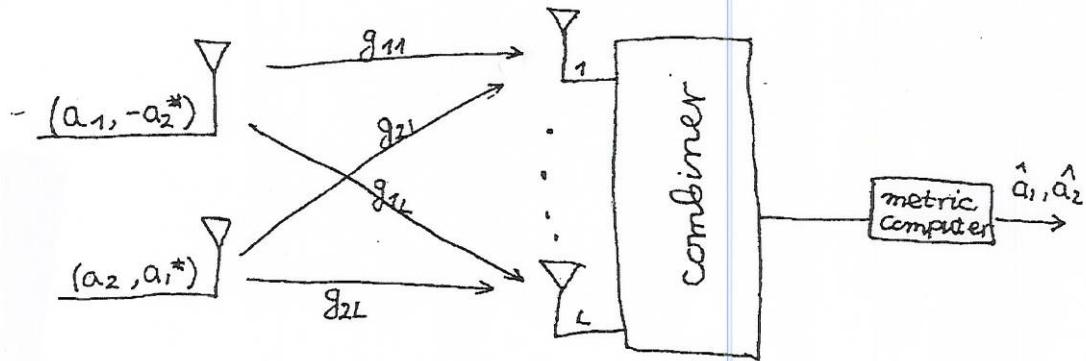
$$\begin{aligned}
 \nabla_{\underline{W}} \operatorname{Re} \left\{ \bar{\Phi}_{\tilde{s}_0 \tilde{r}_t} \underline{W}^* \right\} &= \nabla_{\underline{W}_R} \operatorname{Re} \left\{ \bar{\Phi}_{\tilde{s}_0 \tilde{r}_t} \underline{W}^* \right\} + j \nabla_{\underline{W}_I} \operatorname{Re} \left\{ \bar{\Phi}_{\tilde{s}_0 \tilde{r}_t} \underline{W}^* \right\} \\
 &= \bar{\Phi}_{\tilde{s}_0 \tilde{r}_t R} + j \bar{\Phi}_{\tilde{s}_0 \tilde{r}_t I} \\
 &= \bar{\Phi}_{\tilde{s}_0 \tilde{r}_t}
 \end{aligned}$$

$$\begin{aligned}
 \nabla_{\underline{W}} \underline{W}^T \bar{\Phi}_{\tilde{r}_t \tilde{r}_t} \underline{W}^* &= \nabla_{\underline{W}_R} \underline{W}^T \bar{\Phi}_{\tilde{r}_t \tilde{r}_t} \underline{W}^* + j \nabla_{\underline{W}_I} \underline{W}^T \bar{\Phi}_{\tilde{r}_t \tilde{r}_t} \underline{W}^* \\
 &= 2 \underline{W}_R^T \bar{\Phi}_{\tilde{r}_t \tilde{r}_t R} - 2 \underline{W}_I^T \bar{\Phi}_{\tilde{r}_t \tilde{r}_t I} \\
 &\quad + j (2 \underline{W}_I^T \bar{\Phi}_{\tilde{r}_t \tilde{r}_t R} + 2 \underline{W}_R^T \bar{\Phi}_{\tilde{r}_t \tilde{r}_t I}) \\
 &= 2 (\underline{W}_R^T + j \underline{W}_I^T) (\bar{\Phi}_{\tilde{r}_t \tilde{r}_t R} + j \bar{\Phi}_{\tilde{r}_t \tilde{r}_t I}) \\
 &= 2 \underline{W}^T \bar{\Phi}_{\tilde{r}_t \tilde{r}_t}
 \end{aligned}$$

Finally,

$$\nabla_{\underline{W}} J = 2 \underline{W}^T \bar{\Phi}_{\tilde{r}_t \tilde{r}_t} - 2 \bar{\Phi}_{\tilde{s}_0 \tilde{r}_t}$$

6.19 2xL Alamouti's combiner



g_{ij} - channel gain between transmit antenna i and receiver antenna j

$r_j^{(1)}$ - received signal at antenna j at time t

$r_j^{(2)}$ - received signal at antenna j at time $t+T$

The encoding scheme is:

→ symbols a_1 and a_2 are transmitted from antennas 1 and 2 at time t

→ symbols $-a_2^*$ and a_1^* are transmitted from antennas 1 & 2 at time $t+T$

The received signals are

$$r_1^{(1)} = g_{11} a_1 + g_{21} a_2 + n_1^{(1)}$$

$$r_2^{(1)} = g_{12} a_1 + g_{22} a_2 + n_2^{(1)}$$

$$\vdots \quad \vdots \quad \vdots \quad \vdots$$

$$r_L^{(1)} = g_{1L} a_1 + g_{2L} a_2 + n_L^{(1)}$$

$$r_1^{(2)} = g_{11} (-a_2^*) + g_{21} a_1^* + n_1^{(2)} \Leftrightarrow r_1^{(2)*} = -g_{11}^* a_2 + g_{21}^* a_1 + n_1^{(2)*}$$

$$\vdots \quad \vdots \quad \vdots \quad \vdots$$

$$r_L^{(2)} = g_{1L} (-a_2^*) + g_{2L} a_1^* + n_L^{(2)} \Leftrightarrow r_L^{(2)*} = -g_{1L}^* a_2 + g_{2L}^* a_1 + n_L^{(2)*}$$

The combiner constructs two signal vectors:

$$v_1 = g_{11}^* r_1^{(1)} + g_{12}^* r_2^{(1)} + \dots + g_{1L}^* r_L^{(1)} + g_{21}^* r_1^{(2)*} + \dots + g_{2L}^* r_L^{(2)*}$$

$$v_2 = g_{21}^* r_1^{(1)} + g_{22}^* r_2^{(1)} + \dots + g_{2L}^* r_L^{(1)} - g_{11} r_1^{(2)*} - \dots - g_{1L} r_L^{(2)*}$$

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6.20 We employ Alamouti's scheme on a per subcarrier basis. That is, treat each subcarrier independently.

Transmit OFDM symbol

